

APPLICATION
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TITLE: INDIVIDUAL JET VOLTAGE TRIMMING CIRCUITRY
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INDIVIDUAL VOLTAGE TRIMMING

BACKGROUND

The invention relates to droplet ejection devices.

Inkjet printers are one type of apparatus employing droplet ejection devices. In one type of inkjet printer, ink drops are delivered from a plurality of linear inkjet print head devices oriented perpendicular to the direction of travel of the substrate being printed. Each print head device includes a plurality of droplet ejection devices formed in a monolithic body that defines a plurality of pumping chambers (one for each individual droplet ejection device) in an upper surface and has a flat piezoelectric actuator covering each pumping chamber. Each individual droplet ejection device is activated by a voltage pulse to the piezoelectric actuator that distorts the shape of the piezoelectric actuator and discharges a droplet at the desired time in synchronism with the movement of the substrate past the print head device.

Each individual droplet ejection device is independently addressable and can be activated on demand in proper timing with the other droplet ejection devices to generate an image. Printing occurs in print cycles. In each print cycle, a fire pulse (e.g., 150 volts) is applied to all of the droplet ejection devices at the same time, and enabling signals are sent to only the individual droplet ejection devices that are to jet ink in that print cycle.

SUMMARY OF THE INVENTION

The invention features, in general, apparatus including a plurality of droplet ejection devices, an electric source and a controller. Each droplet ejection device includes a fluid chamber having an ejection nozzle, an electrically actuated displacement device associated with the chamber, and a switch having an input connected to the electric source, an output connected to the electrically actuated displacement device, and a control signal input that is controlled by the controller to control whether the input (and thus the electric source) is connected to the output (and thus the electrically actuated device). The electrically actuated displacement device moves between a displaced position and an undisplaced position to change the volume of the chamber as a capacitance associated with the electrically actuated displacement device changes in charge between an actuated condition and an unactuated condition. The controller provides respective charge control signals to respective control signal inputs to control the extent of

change in charge on respective capacitances by the time that the respective switch connects the electrical signal to the respective electrically actuated displacement device.

Particular embodiments of the invention may include one or more of the following features.

5 The actuated condition of the electrically actuated displacement device corresponds to a charged condition, and the unactuated condition corresponds to an uncharged condition. The controller controls the extent of charge placed on respective capacitances by the time that the respective the switch connects the electrical signal to the respective electrically actuated displacement device. Each droplet ejection device can also include a second switch that has a
10 second input connected to a discharging electrical terminal, a second output connected to the electrically actuated displacement device, and a second control signal input to determine whether the second input is connected to or disconnected from the second output, and the controller can provide respective discharge control signals to respective second control signal inputs to control discharge of the charge on respective capacitances.

15 Each droplet ejection device can include a first resistance between the electric source and the electrically actuated displacement device. Each droplet ejection device can include a second resistance between the discharging electrical terminal and the electrically actuated displacement device.

20 The first resistance can be between the electrical source and the electrically actuated displacement device and can be external of an electrical path from the electrically actuated displacement device to the second switch, and the second resistance can be included in the electrical path from the electrically actuated device to the discharging electrical terminal. Alternatively, a single resistance can be used to charge and discharge a respective capacitance. A plurality of resistors, voltages and switches can be connected to each electrically actuated
25 displacement device and controlled by the controller to change the charge on the capacitance. The discharging electrical terminal can be at ground. The electrical signal can be a controlled voltage signal, a controlled current signal, or a constant current.

30 When the first control signal is a constant voltage, the first control signal can terminate the connection of the constant voltage to the electrically actuated displacement device when the charge on the electrically actuated displacement device is at a predetermined value which is less

than the constant voltage. The electrically actuated displacement device can be a piezoelectric actuator.

The control signal(s) can be controlled to provide uniform droplet volumes or velocities from the plurality of droplet ejection devices. The control signal(s) can be controlled to provide
5 predetermined different drop volumes or velocities from different droplet ejection devices so as to provide gray scale control. The first and second control signals can be controlled to connect the electrical signal to respective electrically actuated displacement devices for respective predetermined times. A control signal can be controlled to connect the electrical signal to
10 respective electrically actuated displacement devices until respective electrically actuated displacement devices achieve respective predetermined charge voltages. The control signal(s) can be controlled to provide a voltage that is insufficient to eject a droplet, but is sufficient to move a meniscus of a liquid at an ejection nozzle of the droplet ejection device. The control signals can be controlled to inject noise into images being printed so as to break up possible print patterns and banding. The control signals can be controlled to vary the amplitude of charge as
15 well as the length of time of charge on the electrically actuated displacement device for the first droplet out of a droplet ejection device so as to match subsequent droplets.

In particular embodiments the controller adds a delay to a firing pulse for a displacement device when that device and an adjacent device are called upon to both fire at the same time. The leading edge of firing pulse for the delayed device is delayed by the delay amount after the
20 leading edge of the firing pulse of the undelayed displacement device.

The apparatus can be an inkjet print head. The controller can include a field programmable gate array on a circuit board mounted to a monolithic body in which the pumping chambers are formed. The controller can control the first switch as a function of the frequency of droplet ejection to reduce variation in drop volume as a function of frequency.

25 Particular embodiments of the invention may include one or more of the following advantages. The charging up of an actuator to a desired charge and then disconnecting the electric source results in a saving in electricity over driving a device to a voltage and maintaining the voltage. One can also individually control the charge on devices, the slope of the change in charge, and the timing and slope of discharge to achieve various effects such as uniform droplet
30 volume or velocity and gray scale control.

The details of one or more embodiments of the invention are set forth in the accompanying drawings and the description below. Other features, objects, and advantages of the invention will be apparent from the description and drawings, and from the claims.

BRIEF DESCRIPTION OF DRAWINGS

5 Fig. 1 is a diagrammatic view of components of an inkjet printer.

Fig. 2 is a vertical section, taken at 2-2 of Fig. 1, of a portion of a print head of the Fig. 1 inkjet printer showing a semiconductor body and an associated piezoelectric actuator defining a pumping chamber of an individual droplet ejection device of the print head.

10 Fig. 3 is a schematic showing electrical components associated with an individual droplet ejection device.

Fig. 4 is a timing diagram for the operation of the Fig. 3 electrical components.

Fig. 5 is a block diagram of circuitry of a print head of the Fig. 1 printer.

Fig. 6 is a schematic showing an alternative embodiment of electrical components associated with an individual droplet ejection device.

15 Fig. 7 is a timing diagram showing the charge voltage on the capacitance for the actuator for the operation of the Fig. 6 electrical components.

DETAILED DESCRIPTION

20 As shown in Fig. 1, the 128 individual droplet ejection devices 10 (only one is shown on Fig. 1) of print head 12 are driven by constant voltages provided over supply lines 14 and 15 and distributed by on-board control circuitry 19 to control firing of the individual droplet ejection devices 10. External controller 20 supplies the voltages over lines 14 and 15 and provides control data and logic power and timing over additional lines 16 to on-board control circuitry 19. Ink jetted by the individual ejection devices 10 can be delivered to form print lines 17 on a

25 substrate 18 that moves under print head 12. While the substrate 18 is shown moving past a stationary print head 12 in a single pass mode, alternatively the print head 12 could also move across the substrate 18 in a scanning mode.

Referring to Fig. 2, each droplet ejection device 10 includes an elongated pumping chamber 30 in the upper face of semiconductor block 21 of print head 12. Pumping chamber 30

30 extends from an inlet 32 (from the source of ink 34 along the side) to a nozzle flow path in

descender passage 36 that descends from the upper surface 22 of block 21 to a nozzle opening 28 in lower layer 29. A flat piezoelectric actuator 38 covering each pumping chamber 30 is activated by a voltage provided from line 14 and switched on and off by control signals from on-board circuitry 19 to distort the piezoelectric actuator shape and thus the volume in chamber 30 and discharge a droplet at the desired time in synchronism with the relative movement of the substrate 18 past the print head device 12. A flow restriction 40 is provided at the inlet 32 to each pumping chamber 30.

Fig. 3 shows the electrical components associated with each individual droplet ejection device 10. The circuitry for each device 10 includes a charging control switch 50 and charging resistor 52 connected between the DC charge voltage X_{vdc} from line 14 and the electrode of piezoelectric actuator 38 (acting as one capacitor plate), which also interacts with a nearby portion of an electrode (acting as the other capacitor plate) which is connected to ground or a different potential. The two electrodes forming the capacitor could be on opposite sides of piezoelectric material or could be parallel traces on the same surface of the piezoelectric material. The circuitry for each device 10 also includes a discharging control switch 54 and discharging resistor 56 connected between the DC discharge voltage Y_{dc} (which could be ground) from line 15 and the same side of piezoelectric actuator 38. Switch 50 is switched on and off in response to a Switch Control Charge signal on control line 60, and switch 54 is switched on and off in response to a Switch Control Discharge signal on control line 62.

Referring to Figs. 3 and 4, piezoelectric actuator 38 functions as a capacitor; thus, the voltage across piezoelectric actuator ramps up from V_{pzt_start} after switch 50 is closed in response to switch charge pulse 64 on line 60. At the end of pulse 64, switch 50 opens, and the ramping of voltage ends at V_{pzt_finish} (a voltage less than X_{vdc}). Piezoelectric actuator 38 (acting as a capacitor) then generally maintains its voltage V_{pzt_finish} (it may decay slightly as shown in Fig. 4), until it is discharged by connection to a lower voltage Y_{dc} by discharge control switch 54, which is closed in response to switch discharge pulse 66 on line 62. The speeds of ramping up and down are determined by the voltages on lines 14 and 15 and the time constants resulting from the capacitance of piezoelectric actuator 38 and the resistances of resistors 52 and 56. The beginning and end of print cycle 68 are shown on Fig. 4. Pulses 64 and 66 are thus timed with respect to each other to maintain the voltage on piezoelectric actuator 38 for the desired length of time and are timed with respect to the print cycle 68 to eject the droplet at the

desired time with respect to movement of substrate 18 and the ejection of droplets from other ejection devices 10. The length of pulse 64 is set to control the magnitude of V_{pzt} , which, along with the width of the PZT voltage between pulses 64, 66, controls drop volume and velocity. If one is discharging to Y_{vdc} the length of pulse 66 should be long enough to cause the output voltage to get as close as desired to Y_{vdc} ; if one is discharging to an intermediate voltage, the length of pulse 66 should be set to end at a time set to achieve the intermediate voltage.

Referring to Fig. 5, on-board control circuitry 19 includes inputs for constant voltages X_{vdc} and Y_{dc} over lines 14, 15 respectively, D0-D7 data inputs 70, logic level fire pulse trigger 72 (to synchronize droplet ejection to relative movement of substrate 18 and print head 12), logic power 74 and optional programming port 76. Circuitry 19 also includes receiver 78, field programmable gate arrays (FPGAs) 80, transistor switch arrays 82, resistor arrays 84, crystals 86, and memory 88.

Transistor switch arrays 82 each include the charge and discharge switches 50, 54 for 64 droplet ejection devices 10.

FPGAs 80 each include logic to provide pulses 64, 66 for respective piezoelectric actuators 38 at the desired times. D0-D7 data inputs 70 are used to set up the timing for individual switches 50, 54 in FPGAs 80 so that the pulses start and end at the desired times in a print cycle 68. Where the same size droplet will be ejected from an ejection device throughout a run, this timing information only needs to be entered once, over inputs D0-D7, prior to starting a run. If droplet size will be varied on a drop-by-drop basis, e.g., to provide gray scale control, the timing information will need to be passed through D0-D7 and updated in the FPGAs at the beginning of each print cycle. Input D0 alone is used during printing to provide the firing information, in a serial bit stream, to identify which droplet ejection devices 10 are operated during a print cycle. Instead of FPGAs other logic devices, e.g., discrete logic or microprocessors, can be used.

Resistor arrays 84 include resistors 52, 56 for the respective droplet ejection devices 10. There are two inputs and one output for each of 64 ejection devices controlled by an array 84.

Programming port 76 can be used instead of D0-D7 data input 70 to input data to set up FPGAs 80. Memory 88 can be used to buffer or prestore timing information for FPGAs 80.

In operation under a normal printing mode, the individual droplet ejection devices 10 can be calibrated to determine appropriate timing for pulses 64, 66 for each device 10 so that each

device will eject droplets with the desired volume and desired velocity, and this information is used to program FPGAs 80. This operation can also be employed without calibration so long as appropriate timing has been determined. The data specifying a print job are then serially transmitted over the D0 terminal of data input 72 and used to control logic in FPGAs to trigger pulses 64, 66 in each print cycle in which that particular device is specified to print in the print job.

In a gray scale print mode, or in operations employing drop-by-drop variation, information setting the timing for each device 10 is passed over all eight terminals D0-D7 of data input 70 at the beginning of each print cycle so that each device will have the desired drop volume during that print cycle.

FPGAs 80 can also receive timing information and be controlled to provide so-called tickler pulses of a voltage that is insufficient to eject a droplet, but is sufficient to move the meniscus and prevent it from drying on an individual ejection device that is not being fired frequently.

FPGAs 80 can also receive timing information and be controlled to eject noise into the droplet ejection information so as to break up possible print patterns and banding.

FPGAs 80 can also receive timing information and be controlled to vary the amplitude (i.e., V_{pzt_finish}) as well as the width (time between charge and discharge pulses 64, 66) to achieve, e.g., a velocity and volume for the first droplet out of an ejection device 10 as for the subsequent droplets during a job.

The use of two resistors 52, 56, one for charge and one for discharge, permits one to independently control the slope of ramping up and down of the voltage on piezoelectric actuator 38. Alternatively, the outputs of switches 50, 54 could be joined together and connected to a common resistor that is connected to piezoelectric actuator 38 or the joined together output could be directly connected to the actuator 38 itself, with resistance provided elsewhere in series with the actuator 38.

By charging up to the desired voltage (V_{pzt_finish}) and maintaining the voltage on the piezoelectric actuators 38 by disconnecting the source voltage X_{vdc} and relying on the actuator's capacitance, less power is used by the print head than would be used if the actuators were held at the voltage (which would be X_{vdc}) during the length of the firing pulse.

Other embodiments of the invention are within the scope of the appended claims. E.g., a switch and resistor could be replaced by a current source that is switched on and off. Also, common circuitry (e.g., a switch and resistor) could be used to drive a plurality of droplet ejection devices. Also, the drive pulse parameters could be varied as a function of the frequency of droplet ejection to reduce variation in drop volume as a function of frequency. Also, a third switch could be associated with each pumping chamber and controlled to connect the electrode of the piezoelectric actuator 38 to ground, e.g., when not being fired, while the second switch is used to connect the electrode of the piezoelectric actuator 38 to a voltage lower than ground to speed up the discharge.

It is also possible to create more complex waveforms. For example, switch 50 could be closed to bring the voltage up to V1, then opened for a period of time to hold this voltage, then closed again to go up to voltage V2. A complex waveform can be created by appropriate closings of switch 50 and switch 54.

Multiple resistors, voltages, and switches could be used per droplet ejection device to get different slew rates as shown in Figs. 6 and 7. Fig. 6 shows an alternative control circuit 100 for an injection device in which multiple (here two) charging control switches 102, 104 and associated charging resistors 106, 108 are used to charge the capacitance 110 of the piezoelectric actuator and multiple (here two) discharging control switches 112, 114 and associated discharging resistors 116, 118 are used to discharge the capacitance. Fig. 7 shows the resulting voltage charge on the capacitance. The ramp up at 120 is caused by having switch 102 closed while the other switches are open. The ramp up at 122 is caused by having switch 104 closed while the other switches are open. The ramp down at 124 is caused by having switch 112 closed while the other switches are open. The ramp down at 126 is caused by having switch 114 closed while the other switches are open.